

Mathematical Modelling of Wastewater Treatment Plants

Part II: The Modelling Process

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Outline

- Types of models
- Modeling strategy
- System identification (parameter identification)
- Example of a simple two-state variable dynamic system

References:

Olsson, G. and Newell, B. (1999). Wastewater Treatment Systems. IWA Publishing, 742 p.
Jeppsson, U. (1996). Modelling Aspects of Wastewater Treatment Processes. Ph.D. Thesis, Lund University, 428 p.



Types of models

- Lab/bench scale models
- Physical models
- Mathematical models
- Qualitative models
- Linguistic models
- Visual models



Mathematical models

- A mathematical model is a representation (simplification) of reality, designed to help us understand the processes that are taking place in the plant
- To represent the same process, models can be very simple or they can be extremely complex
- From an engineering perspective, models should be “as simple as possible, but no simpler”
- Need to be concerned with model
« identifiability »

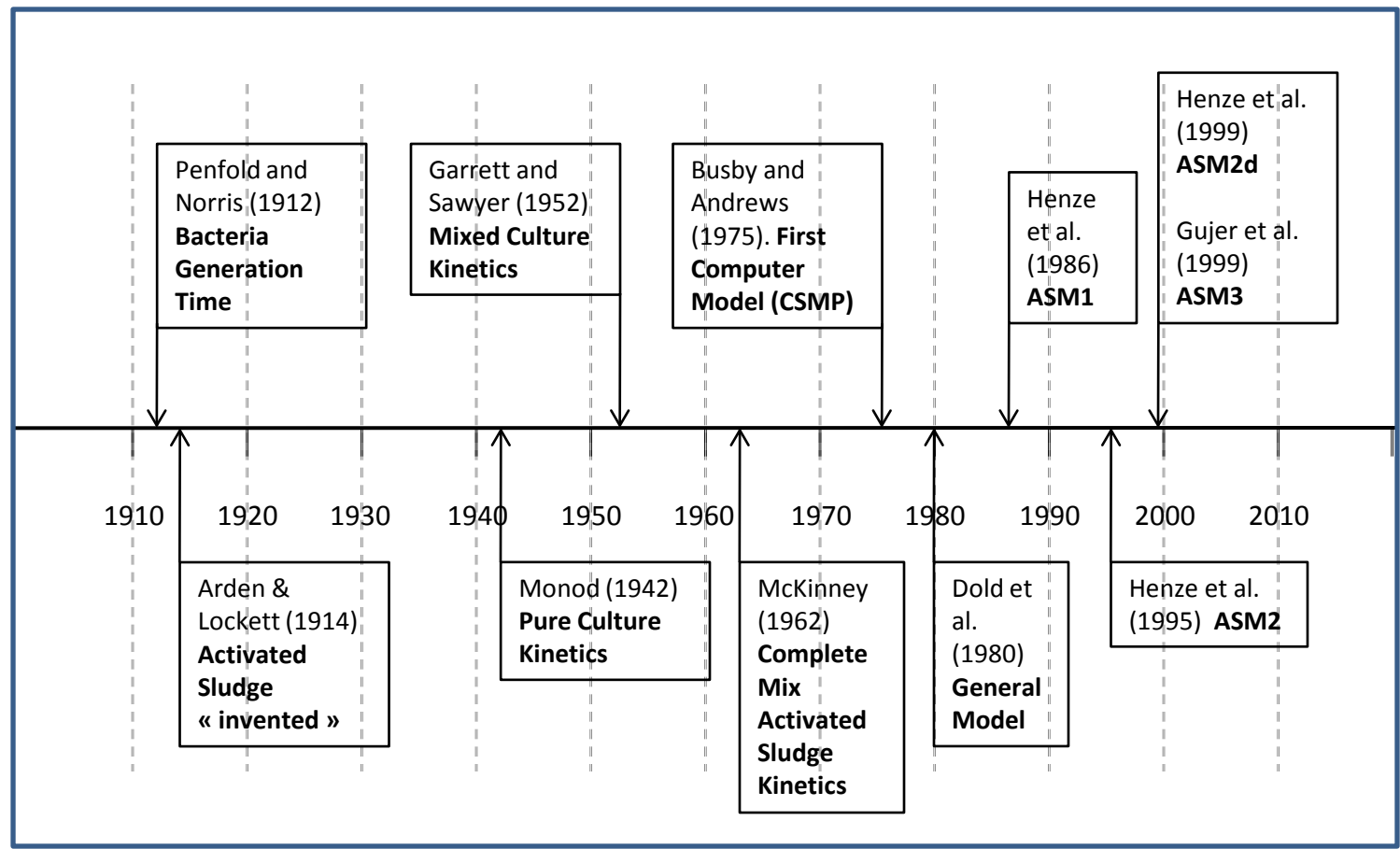


Mathematical models

- The objective is to conceptualize our knowledge of a process or a physical system in a mathematical description of the process
- Once we have a working model we can use it for:
 - Design
 - Operation
 - Research
 - Performance assessment / plant audit
 - Training of operators
 - Forecast and planning purposes
- Modelling of the activated sludge process is not new ...

Activated Sludge Modeling Timeline

(adapted from Bruce Johnson, CH2M Hill, 2009)



Empirical Design,
Piloting & Guesswork

Kinetics-
Based Design

Whole Plant
Simulators



Modelling Strategy

1. Functional process specification
2. Define your modelling objectives
 - a. Purpose
 - b. Accuracy
 - c. Boundary conditions
 - d. Time-scale
 - e. Etc.
3. Model type (L vs NL, D vs Continuous, etc.)
4. Model development
5. Model verification
6. Model calibration / validation
7. Use the model for its intended purpose



Modelling Objectives

1. Define the purpose of the model (what will it be used for?)
 - Design
 - Research
 - Process control and operation
 - Forecasting
 - Performance analysis / audit
 - Education / learning / training
 - Etc.
 - A design-based model will be very different than a model developed for research purposes (e.g., CAPDETWorks vs GPS-X)
 - Hierarchical modeling (a hierarchy of models)
2. Define System Boundaries
 - A component of a reactor
 - The reactor itself
 - Liquid line
 - Entire plant (liquid and sludge line processes)



Modelling Objectives

3. Define time scale of interest

- Dynamics of processes will vary from

seconds & minutes (e.g., dissolved oxygen dynamics)

to

days and/or weeks (biomass growth)

Depending on your modeling objectives, model formulation and solution will be dependent on the time scale of interest

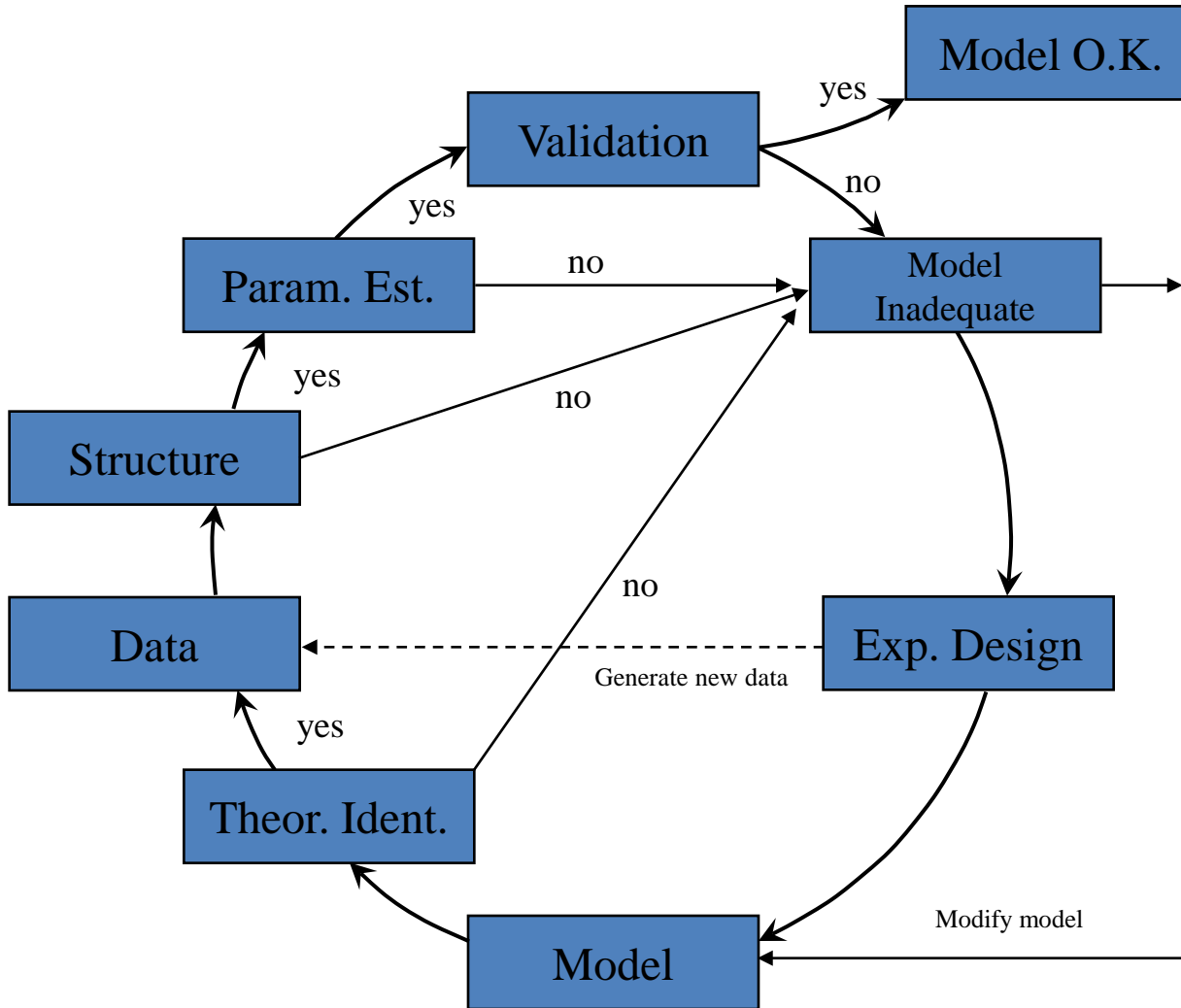
4. Define the desired accuracy



Model Type

- Mechanistic vs Black-Box (I/O or ARMAX)
- Deterministic vs stochastic
- Continuous vs discrete
- Distributed vs lumped
- Time domain vs frequency domain

Mechanistic, deterministic, time-domain, continuous distributed models



Adapted from Jeppsson (1996)



System Identification

- Are the model parameters identifiable?
 - Are they uniquely identifiable ? i.e., is there a unique solution?
 - Are they locally identifiable ? i.e., finite number of solutions, i.e., parameter values
 - Are they unidentifiable ? i.e.,



A Simple Example – Two-State Variable System

Substrate S ; Biomass X

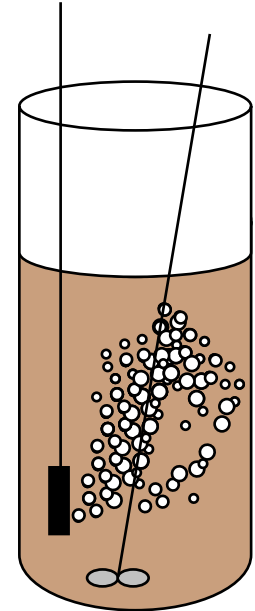
Consider:

$$\frac{dX}{dt} = \mu(S)X - bX \quad (1)$$

$$\frac{dS}{dt} = -\frac{1}{Y}\mu(S)X \quad (2)$$

$$\mu(S) = \frac{\hat{\mu}S}{K_s + S} \quad (3)$$

Assume X and S are measurable.



Can all 4 parameters K_s , $\hat{\mu}$, Y , b

be uniquely determined from perfect data? In other words, is the system globally identifiable?



Let $X_0 = X(0)$; $S_0 = S(0)$

$$X'(0) = \frac{\hat{\mu}S_0}{K_s + S_0} X_0 - bX_0 = X_1 \quad (4)$$

$$S'(0) = -\frac{1}{Y} \frac{\hat{\mu}S_0}{K_s + S_0} X_0 = S_1 \quad (5)$$

$$\mu = \frac{\hat{\mu}S_0}{K_s + S_0}$$

$$X_1 = (\mu - b)X_0$$

$$S_1 = -\frac{\mu}{Y} X_0$$



Take the first-order Taylor series expansion of Eq. (1) and (2) at time $t=0$

$$X''(0) = (\mu - b)X_1 + \frac{\mu K_S X_0 S_1}{(K_S + S_0)S_0} = X_2 \quad (6)$$

$$S''(0) = -\frac{\mu}{Y} \left(X_1 + \frac{\mu K_S X_0 S_1}{(K_S + S_0)S_0} \right) = S_2 \quad (7)$$

Solve (4), (5), (6) and (7) for K_S , $\hat{\mu}$, Y , b



Solve for parameters

$$K_S = \frac{S_2 S_0^2 X_0 - S_1 S_0^2 X_1}{S_1^2 X_0 - S_2 S_0 X_0 + S_1 S_0 X_1}$$

$$\mu = \frac{X_2 X_0 S_1 - X_1^2 S_1}{S_2 X_0^2 - S_1 X_1 X_0}$$

$$\hat{\mu} = \frac{(X_2 X_0 S_1 - X_1^2 S_1)(K_S + S_0)}{S_2 S_0 X_0^2 - S_1 S_0 X_1 X_0}$$

$$b = \frac{S_1 X_2 - S_2 X_1}{S_2 X_0 - S_1 X_1}$$

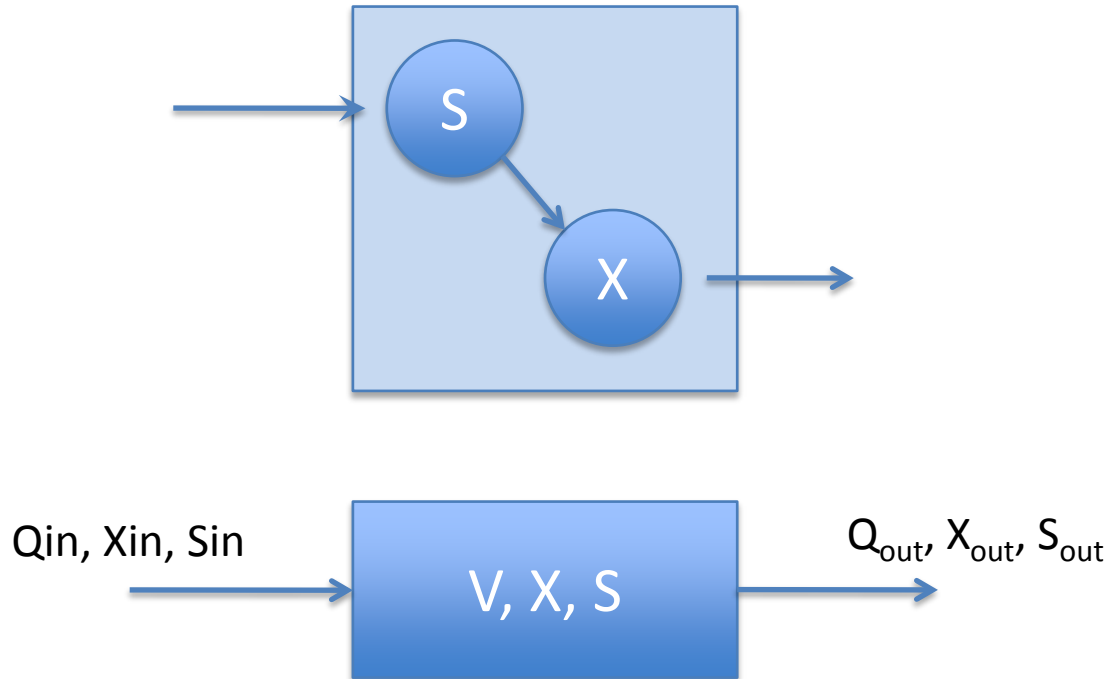
$$Y = \frac{X_1^2 - X_1 X_0}{S_2 X_0 - S_1 X_1}$$

Accordingly, the process parameters are identifiable.

If measurements are noise-corrupted
Then parameters are not uniquely
Identifiable!



Modelling of a Single Substrate System



$Q_{in} = Q_{out} = Q \rightarrow$ Constant Volume Reactor

Input – Output = Accumulation - Reaction



- Biomass (X_H):

$$QX_{H,in} - QX_{H,out} = \frac{d(VX_H)}{dt} - r_H V$$

$$r_{X_H} = \hat{\mu} \left(\frac{S_S}{K_S + S_S} \right) X_H$$

$$X_{H,in} = 0$$

$$\text{CSTR} \rightarrow X_{H,out} = X_H$$

$$\frac{dX_H}{dt} = \left(\hat{\mu} \left(\frac{S_S}{K_S + S_S} \right) X_H - \frac{X_H}{\theta} \right)$$

- Substrate (S_S):

$$QS_{S,in} - QS_{S,out} = \frac{d(VS_S)}{dt} - r_S V$$

$$r_{S_S} = -\frac{1}{Y_H} \hat{\mu} \left(\frac{S_S}{K_S + S_S} \right) X_H$$

$$\text{CSTR} \rightarrow S_{S,out} = S_S$$

$$\frac{dS_S}{dt} = \frac{1}{\theta} \left((S_{S,in} - S_S) - \frac{1}{Y_H} \hat{\mu} \left(\frac{S_S}{K_S + S_S} \right) X_H \right)$$

Solve these two NODE using numerical methods techniques.

Matlab, Simulink, ACSL, etc.



Two-State / One Process Model in Petersen Matrix Format

Processes ↓	Components (state-variables)		Process rate Kinetics
	Substrate, S_S	Biomass, X_H	
Aerobic heterotrophic growth	$-\frac{1}{Y_H}$	1	$\hat{\mu} \left(\frac{S_S}{K_S + S_S} \right) X_H$



Component →		<i>i</i>	1	2	3	4	5	6	7	8	9	10	11	12	13	Process Rate, ρ_j [ML ⁻³ T ⁻¹]
<i>j</i>	Process ↓		<i>S_I</i>	<i>S_S</i>	<i>X_I</i>	<i>X_S</i>	<i>X_{B,H}</i>	<i>X_{B,A}</i>	<i>X_P</i>	<i>S_O</i>	<i>S_{NO}</i>	<i>S_{NH}</i>	<i>S_{ND}</i>	<i>X_{ND}</i>	<i>S_{ALK}</i>	
1	Aerobic growth of heterotrophs			$\frac{1}{Y_H}$			1			$\frac{1 - Y_H}{Y_H}$		$-i_{XB}$			$\frac{i_{XB}}{14}$	$\hat{\mu}_H \left(\frac{S_S}{K_S + S_S} \right) \left(\frac{S_O}{K_{O,H} + S_O} \right) X_{B,H}$
2	Anoxic growth of heterotrophs			$\frac{1}{Y_H}$			1				$\frac{1 - Y_H}{2.86 Y_H}$	$-i_{XB}$			$\frac{i_{XB}}{14}$	$\hat{\mu}_H \left(\frac{S_S}{K_S + S_S} \right) \left(\frac{K_{O,H}}{K_{O,H} + S_O} \right) \left(\frac{S_{NO}}{K_{NO} + S_{NO}} \right) \eta_g X_{B,H}$
3	Aerobic growth of autotrophs							1		$-\frac{4.57}{Y_A} + 1$	$\frac{1}{Y_A}$	$-i_{XB} - \frac{1}{Y_A}$			$-\frac{i_{XB}}{14} - \frac{1}{7 Y_A}$	$\hat{\mu}_A \left(\frac{S_{NH}}{K_{NH} + S_{NH}} \right) \left(\frac{S_O}{K_{O,A} + S_O} \right) X_{B,A}$
4	'Decay' of heterotrophs					$1 - f_p$	-1		f_p					$i_{XB} - f_p i_{XP}$		$b_H X_{B,H}$
5	'Decay' of autotrophs					$1 - f_p$		-1	f_p					$i_{XB} - f_p i_{XP}$		$b_A X_{B,A}$
6	Ammonification of soluble organic nitrogen											1	-1		$\frac{1}{14}$	$k_a S_{ND} X_{B,H}$
7	'Hydrolysis' of entrapped organics			1		-1										$k_h \frac{X_S / X_{B,H}}{K_X + (X_S / X_{B,H})} \left[\left(\frac{S_O}{K_{O,H} + S_O} \right) + \eta_h \left(\frac{K_{O,H}}{K_{O,H} + S_O} \right) \left(\frac{S_{NO}}{K_{NO} + S_{NO}} \right) \right] X_{B,H}$
8	'Hydrolysis' of entrapped organic nitrogen												1	-1		$\rho_7 (X_{ND} / X_S)$
Observed Conversion Rates [ML ⁻³ T ⁻¹]			$r_i = \sum_j v_{ij} \rho_j$									$r_i = \sum_j v_{ij} \rho_j$				
Stoichiometric Parameters: Heterotrophic yield: Y_H Autotrophic yield: Y_A Fraction of biomass yielding particulate products: f_p Mass N/Mass COD in biomass: i_{XB} Mass N/Mass COD in products from biomass: i_{XP}			Soluble inert organic matter [M(COD)L ⁻³]	Readily biodegradable substrate [M(COD)L ⁻³]	Particulate inert organic matter [M(COD)L ⁻³]	Slowly biodegradable substrate [M(COD)L ⁻³]	Active heterotrophic biomass [M(COD)L ⁻³]	Active autotrophic biomass [M(COD)L ⁻³]	Particulate products arising from biomass decay [M(COD)L ⁻³]	Oxygen (negative COD) [M(-COD)L ⁻³]	Nitrate and nitrite nitrogen [M(N)L ⁻³]	NH ₄ +NH ₃ nitrogen [M(N)L ⁻³]	Soluble biodegradable organic nitrogen [M(N)L ⁻³]	Particulate biodegradable organic nitrogen [M(N)L ⁻³]	Alkalinity - Molar units	Kinetic Parameters: Heterotrophic growth and decay: $\hat{\mu}_H, K_S, K_{O,H}, K_{NO}, b_H$ Autotrophic growth and decay: $\hat{\mu}_A, K_{NH}, K_{O,A}, b_A$ Correction factor for anoxic growth of heterotrophs: η_g Ammonification: k_a Hydrolysis: k_h, K_X Correction factor for anoxic hydrolysis: η_h

Part III

Dynamic Modelling of the Activated Sludge Process (ASM1)